IF YOU ARE SEEING THIS PAGE, PLEASE NOTE:

As of June 2010, all permits having a fact sheet that are going through a modification will have posted in pdf format the modification fact sheet attached to the front of the previous renewal fact sheet.

FACT SHEETS ARE ON NEXT PAGE

If you have any questions regarding this, please contact the NPDES or PPU sections in the Division of Surface Water.

Attached are:

3PE00008 *MD & KD

National Pollutant Discharge Elimination System (NPDES) Permit Program

FACT SHEET

Regarding an NPDES Permit To Discharge to Waters of the State of Ohio for the Warren Water Pollution Control Center

Public Notice No.: 10-09-071 OEPA Permit No.: **3PE00008*MD**

Public Notice Date: September 29, 2010 Application No.: **OH0027987**

Comment Period Ends: October 29, 2010

Name and Address of Facility Where
Name and Address of Applicant:
Discharge Occurs:

City of Warren Warren WPCC
2323 Main Ave. S.W.

Warren, Ohio 44481

Warren, Ohio 44481

Trumbull County

Receiving Water: **Mahoning River**Subsequent

Stream Network: Beaver River

to Ohio River

Introduction

Development of a Fact Sheet for NPDES permits is mandated by Title 40 of the Code of Federal Regulations, Section 124.8 and 124.56. This document fulfills the requirements established in those regulations by providing the information necessary to inform the public of actions proposed by the Ohio Environmental Protection Agency, as well as the methods by which the public can participate in the process of finalizing those actions.

This Fact Sheet is prepared in order to document the technical basis and risk management decisions that are considered in the determination of water quality based NPDES Permit effluent limitations. The technical basis for the Fact Sheet may consist of evaluations of promulgated effluent guidelines, existing effluent quality, instream biological, chemical and physical conditions, and the relative risk of alternative effluent limitations. This Fact Sheet details the discretionary decision-making process empowered to the Director by the Clean Water Act and Ohio Water Pollution Control Law (ORC 6111). Decisions to award variances to Water Quality Standards or promulgated effluent guidelines for economic or technological reasons will also be justified in the Fact Sheet where necessary.

Effluent limits based on available treatment technologies are required by Section 301(b) of the Clean Water Act. Many of these have already been established by U.S. EPA in the effluent guideline regulations (a.k.a. categorical regulations) for industry categories in 40 CFR Parts 405-499. Technology-based regulations for publicly-owned treatment works are listed in the Secondary Treatment Regulations (40 CFR Part 133). If regulations have not been established for a category of dischargers, the director may establish technology-based limits based on best professional judgment (BPJ).

Fact Sheet for NPDES Permit Modification, Warren WPCC, 2010

Ohio EPA reviews the need for water-quality-based limits on a pollutant-by-pollutant basis. Wasteload allocations are used to develop these limits based on the pollutants that have been detected in the discharge, and the receiving water's assimilative capacity. The assimilative capacity depends on the flow in the water receiving the discharge, and the concentration of the pollutant upstream. The greater the upstream flow, and the lower the upstream concentration, the greater the assimilative capacity is. Assimilative capacity may represent dilution (as in allocations for metals), or it may also incorporate the break-down of pollutants in the receiving water (as in allocations for oxygen-demanding materials).

The need for water-quality-based limits is determined by comparing the wasteload allocation for a pollutant to a measure of the effluent quality. The measure of effluent quality is called PEQ - Projected Effluent Quality. This is a statistical measure of the average and maximum effluent values for a pollutant. As with any statistical method, the more data that exists for a given pollutant, the more likely that PEQ will match the actual observed data. If there is a small data set for a given pollutant, the highest measured value is multiplied by a statistical factor to obtain a PEQ; for example if only one sample exists, the factor is 6.2, for two samples - 3.8, for three samples - 3.0. The factors continue to decline as samples sizes increase. These factors are intended to account for effluent variability, but if the pollutant concentrations are fairly constant, these factors may make PEQ appear larger than it would be shown to be if more sample results existed.

Summary of Permit Conditions

This permit modification would change monitoring requirements for the WPCC in response to the introduction of "low salinity" wastewater from Marcellus Shale hydrofracturing. The proposed inputs to the WPCC are 100,000 gallons per day (0.1 million gallons per day) at concentrations of total dissolved solids less than or equal to 50,000 mg/l. Additions to the WPCC at this magnitude will not cause significant degradation to the Mahoning River. As a result, Ohio EPA is requiring only monitoring for total dissolved solids, sulfate and chloride. The monitoring frequency for TDS would increase to daily to track any significant variation in effluent concentrations due to the new salty inputs. Sulfate, chloride, barium and strontium are new parameters in the permit; these have been added to measure the specific materials that make up TDS.

Ohio EPA is also proposing to increase the effluent toxicity monitoring requirement from 1/year to 1/quarter to check the effect of TDS discharges on aquatic life.

Procedures for Participation in the Formulation of Final Determinations

The proposed modification is tentative but shall become final on the effective date unless (1) an adjudication hearing is requested, (2) the Director withdraws and revises the proposed modification after consideration of the record of a public meeting or written comments, or (3) upon disapproval by the Administrator of the U.S. Environmental Protection Agency.

Within thirty (30) days of <u>publication</u> of this notice, any person may submit written comments, a statement as to why the proposed modification should be changed, a request for a public meeting on the proposed modification and/or a request for notice of further actions concerning the modification. All communications timely received will be considered in the final formulation of the modification. If significant public interest is shown a public meeting will be held prior to finalization of the modification.

Within thirty (30) days of the <u>issuance</u> of the proposed modification notice any officer of an agency of the state or of a political subdivision, acting in his representative capacity or any person aggrieved or adversely affected by issuance of it may request an adjudication hearing by submitting a written objection in accordance with Ohio Revised Code Section 3745.07. Since all other conditions of the permit remain in effect, a hearing may not be requested on any issues other than the proposed modification. If an adjudication hearing is requested, the existing NPDES permit will remain in effect until the hearing is resolved. Following the finalization of the modification by the Director, any person who was a party to an adjudication hearing may appeal to the Environmental Review Appeals Commission.

Requests for public meetings shall be in writing and shall state the action of the Director objected to, the questions to be considered, and the reasons the action is contested. Such requests should be addressed to:

Legal Records Section
Ohio Environmental Protection Agency
Lazarus Government Center
P.O. Box 1049
Columbus, Ohio 43216-1049

Interested persons are invited to submit written comments upon the proposed modification. Comments should be submitted in person or by mail no later than 30 days after the date of this Public Notice. Deliver or mail all comments to:

Ohio Environmental Protection Agency Attention: Division of Surface Water Permits and Compliance Section Lazarus Government Center P.O. Box 1049 Columbus, Ohio 43216-1049

The OEPA permit number and Public Notice numbers should appear on each page of any submitted comments. All comments received no later than 30 days after the date of the Public Notice will be considered.

Citizens may conduct file reviews regarding specific companies or sites. Appointments are necessary to conduct file reviews, because requests to review files have increased dramatically in recent years. The first 250 pages copied are free. For requests to copy more than 250 pages, there is a five-cent charge for each page copied. Payment is required by check or money order, made payable to Treasurer State of Ohio.

For additional information about this fact sheet or the proposed modification, contact Erm Gomes at (330) 963-1196 (email: erm.gomes@epa.ohio.gov) or Eric Nygaard at (614) 644-2024 (email: eric.nygaard@epa.ohio.gov)

Location of Discharge/Receiving Water Use Classification

The Warren WPCC discharges to the Mahoning River at River Mile 35.25. The approximate location of the facility is shown in Figure 1.

The Mahoning River, which flows into the Beaver River in Pennsylvania, has the following designated uses: Warmwater Habitat, Agricultural Water Supply, Industrial Water Supply, and Primary Contact Recreation. This section of the Mahoning River is identified by Ohio EPA River Code:18-001, and USEPA River Reach number 05030101-007.

Use designations define the goals and expectations of a waterbody. These goals are set for aquatic life protection, recreation use and water supply use, and are defined in the Ohio WQS (OAC 3745-1-07). The use designations for individual waterbodies are listed in rules -08 through -32 of the Ohio WQS. Once the goals are set, numeric water quality standards are developed to protect these uses. Different uses have different water quality criteria.

Use designations for aquatic life protection include habitats for coldwater fish and macroinvertebrates, warmwater aquatic life and waters with exceptional communities of warmwater organisms. These uses all meet the goals of the federal Clean Water Act. Ohio WQS also include aquatic life use designations for waterbodies which can not meet the Clean Water Act goals because of human-caused conditions that can not be remedied without causing fundamental changes to land use and widespread economic impact. The dredging and clearing of some small streams to support agricultural or urban drainage is the most common of these conditions. These streams are given Modified Warmwater or Limited Resource Water designations.

Recreation uses are defined by the depth of the waterbody and the potential for wading or swimming. Uses are defined for bathing waters, swimming/canoeing (Primary Contact) and wading only (Secondary Contact generally waters too shallow for swimming or canoeing).

Water supply uses are defined by the actual or potential use of the waterbody. Public Water Supply designations apply near existing water intakes so that waters are safe to drink with standard treatment. Most other waters are designated for agricultural and industrial water supply.

Facility Description

The Warren WPCC has a 16.0 MGD design flow and was last upgraded to advanced secondary treatment in February 1988. Treatment processes include grit removal, detritus setting tanks, extended aeration activated sludge, primary and final settling tanks, chlorination, and post aeration with the discharge to the mainstem at

river mile (RM) 35.25. The sewage system is considered separate, but has had a history of problems with sanitary sewer overflows (SSOs) due to excessive inflow/infiltration (I/I).

Ten significant industrial users contribute approximately 3.4 MGD of flow to the treatment works. Eight of these industrial users are categorical industries (subject to U.S. EPA treatment technology regulations). The City of Warren has an approved pretreatment program to regulate these discharges.

Receiving Water Quality / Environmental Hazard Assessment

No recent biological and chemical data exist for this segment of the Mahoning River. Historical data (from 1994) show that this river segment did not meet the designated warmwater habitat aquatic life use. Ohio EPA believes that this non-attainment continues to exist, based on limited biological sampling from 2002 and 2003, along with historical chemical data on stream sediments and recent fish tissue chemistry.

The summary sheet from Ohio's 2006 Integrated Water Quality Monitoring and Assessment Report is attached to this fact sheet. The complete Integrated Report can be found on the Agency website at: http://www.epa.state.oh.us/dsw/tmdl/2006IntReport/2006OhioIntegratedReport.html.

Basis for Modification/Effluent Limits and Permit Conditions

The City of Warren is requesting authorization to accept pretreated wastewater generated during oil and gas well drilling, development, and production. The wastewater would be discharged from regulated centralized waste treatment (CWT) facilities which are tributary to the Warren WPCC. These wastewaters typically contain high levels of Total Dissolved Solids (TDS), and include pollutants such as chlorides, sulfates and barium. While some incidental removal will occur, municipal wastewater treatment plants are not typically designed to treat for TDS. Rather, these facilities rely on their dilution capacity to manage wastes with elevated TDS concentrations. Hence, these pollutants, if not properly controlled, can diminish or inhibit biological treatment processes, pass through the treatment plant, increase effluent toxicity, and cause water quality issues in receiving streams.

Currently, there is limited information on the TDS concentrations in all Mahoning River dischargers. In order to better evaluate the potential impacts on the Warren WPCC and the Mahoning River, the facility conducted an eight week pilot study. Gas well wastewater was introduced, at a controlled rate, into the headworks and pollutants of concern were monitored at defined influent, effluent, biosolids, and upstream and downstream sampling locations. The test was limited to wastewater characterized as "low salinity", i.e. wastewater with a TDS concentration equal to or less than 50,000 mg/l, and the maximum amount introduced into the facility was 100,000 gallons/day. Data was collected during the test on parameters that included TDS, chlorides, barium, strontium, and whole effluent toxicity. Additionally, data was collected for certain radiological parameters.

The results of the pilot study did not show any negative impacts on the treatment plant operations, sludge quality, or effluent toxicity.

Calculations indicate that instream TDS concentrations should increase by approximately 60 mg/l under low flow conditions (i.e. 7Q10). This projected increase should not result in any biological impact to the Mahoning River. Also, it should not impact the public water supply for Beaver Falls, PA, which is located on the Beaver River. Therefore, Ohio EPA is proposing NPDES permit modifications based on a maximum discharge of 100,000 gpd at 50,000 mg/l from gas well wastewater treatment facilities. At these input rates,

the WPCC will not have the reasonable potential to contribute to an exceedance of WQS in the Mahoning River.

To track the progress of these discharges Ohio EPA has added daily effluent monitoring requirements for total dissolved solids. The Agency has also added monitoring requirements for the more important constituent parts of dissolved solids, chloride and sulfate, as well as parameters that are elevated in many ground waters (barium and strontium). Ohio EPA is also proposing to increase the frequency of toxicity monitoring from 1/year to 1/quarter. These additional monitoring requirements assist with assessing potential problems associated with TDS discharges.

Ohio EPA has also added a compliance schedule item that requires Warren to submit an annual report on wastewaters received from these dischargers. This condition also requires the City to stop accepting wastewater if these wastewaters cause inhibition of the plant's biological treatment process, cause water quality impacts downstream of the facility, or adversely affect the quality of the plant's biosolids. These requirements provide an additional check on the inputs of pollutants in this wastewater and action items to minimize environmental impact.

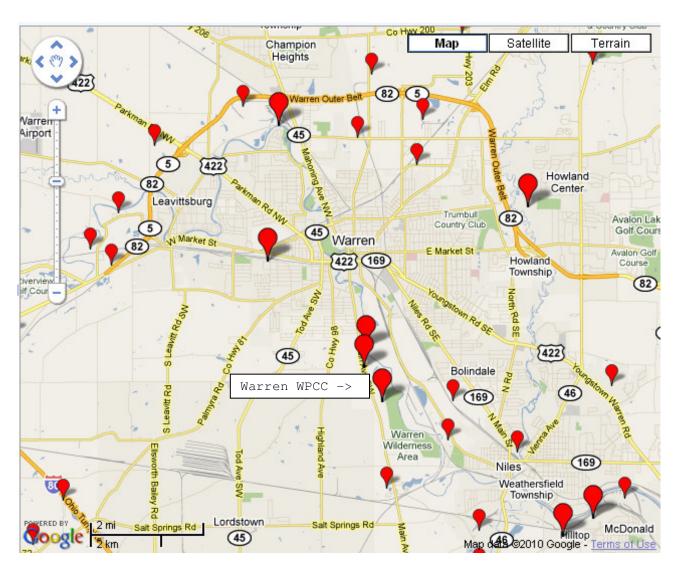


Figure 1. Location of Warren WPCC. Balloons indicate NPDES permittees; the larger balloons show major permittees.

Table 1. Final effluent limits and monitoring requirements for Warren WPCC outfall 3PE00008001 and the basis for their recommendation.

			Effluent Lim			
		Concentrat		Loading (k		
Doromotor	Unito	30 Day	Daily Maximum	30 Day	Daily Maximum	Basis ^b
Parameter	Units	Average	Maximum	Average	Maximum	Dasis
Flow	MGD		Monitor			\mathbf{M}^{c}
Temperature	$^{\circ}$ C		Monitor			M^{c}
Dissolved Oxygen	mg/l		5.0 min.			WQS/PD
COD	mg/l		Monitor	. – – – – – –		M^{c}
$CBOD_5$	mg/l	12	18 ^d	727	1090 ^d	EP/PD
Suspended Solids	mg/l	20	30 ^d	1211	1817 ^d	EP/PD
Ammonia-N	mg/l					
Summer		3.0	4.5 ^d	182	273 ^d	WLA/EP/PD
Winter		15	22 ^d	908	1332 ^d	WLA/EP/PD
Nitrate/Nitrite-N	mg/l		Monitor	·		M^{c}
Kjeldahl-N, T.	mg/l		Monitor	·		M^{c}
Phosphorus	mg/l		Monitor	·		M^{c}
Dissolved Solids	mg/l		Monitor	·		M/RP ^c
Oil and Grease	mg/l		10			WQS
pН	S.U.		6.5 to 9	9.0		WQS
Fecal coliform	#/100ml					
Summer		1000	2000 ^d			WQS
Chlorine Residual	mg/l		0.028			ABS/EP
Cyanide, Free	mg/l	0.024	0.086	1.45	5.21	WLA
Chloride	mg/l		Monitor			M/RP ^c
Sulfate	mg/l		Monitor	. – – – – – –		M/RP ^c
Barium	μg/l		Monitor			M/RP ^c
Cadmium, T. R.	μg/l		Monitor			\mathbf{M}^{c}
Chromium, T. R.	μg/l		Monitor	. – – – – – –		M^{c}
Hex. Chromium						
(Dissolved)	μg/l		Monitor			M^{c}
Copper, T. R.	μg/l		Monitor	. – – – – – –		M^{c}
Lead, T. R.	μg/l		Monitor	·		\mathbf{M}^{c}
Mercury, T.	ng/l		Monitor	·		M^{c}
Nickel, T. R.	μg/l		Monitor	·		\mathbf{M}^{c}
Selenium, T. R.	μg/l		Monitor	·		M^{c}
Strontium	μg/l		Monitor	·		M/RP ^c
Zinc, T. R.	μg/l		Monitor			M^{c}
Whole Effluent	. •					
Toxicity						
Acute	TUa		Monitor (w/o	trigger)		FAR, BPJ
Chronic	TUc		Monitor (w/o			FAR, BPJ
			-			

Table 1. Con't.

^a Effluent loadings based on average design discharge flow of 16 MGD.

Definitions:

ABS = Antibacksliding Rule (OAC 3745-33-05(E) and 40 CFR Part 122.44(I)); EP = Existing Permit; FAR = Federal Application Requirement under 40 CFR 122.21(j); M = Monitoring; PD = Plant Design Criteria; RP = Reasonable Potential for requiring water quality-based effluent limits and monitoring requirements in NPDES permits (3745-33-07(A)); WET = Whole Effluent Toxicity (OAC 3745-33-07(B)); WLA = Wasteload Allocation procedures (OAC 3745-2); WLA/IMZM = Wasteload Allocation limited by Inside Mixing Zone Maximum; WQS = Ohio Water Quality Standards (OAC 3745-1).

- ^c Monitoring of flow and other indicator parameters is specified to assist in the evaluation of effluent quality and treatment plant performance.
- ^d 7 day average limit.

National Pollutant Discharge Elimination System (NPDES) Permit Program

FACT SHEET

Regarding an NPDES Permit To Discharge to Waters of the State of Ohio for the Warren Water Pollution Control Center

Public Notice No.: 08-03-006 OEPA Permit No.: **3PE00008*KD**Public Notice Date: March 4, 2008 Application No.: **OH0027987**

Comment Period Ends: May 4, 2008

Name and Address of Facility Where

Name and Address of Applicant: Discharge Occurs:

City of Warren Warren WPCC
2323 Main Ave. S.W.

Warren, Ohio 44481 Warren, Ohio 44481

Trumbull County

Receiving Water: **Mahoning River** Subsequent

Stream Network: Beaver River

to Ohio River

Introduction

Development of a Fact Sheet for NPDES permits is mandated by Title 40 of the Code of Federal Regulations, Section 124.8 and 124.56. This document fulfills the requirements established in those regulations by providing the information necessary to inform the public of actions proposed by the Ohio Environmental Protection Agency, as well as the methods by which the public can participate in the process of finalizing those actions.

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Effluent limits based on available treatment technologies are required by Section 301(b) of the Clean Water Act. Many of these have already been established by U.S. EPA in the effluent guideline regulations (a.k.a. categorical regulations) for industry categories in 40 CFR Parts 405-499. Technology-

based regulations for publicly-owned treatment works are listed in the Secondary Treatment Regulations (40 CFR Part 133). If regulations have not been established for a category of dischargers, the director may establish technology-based limits based on best professional judgment (BPJ).

Ohio EPA reviews the need for water-quality-based limits on a pollutant-by-pollutant basis. Wasteload allocations are used to develop these limits based on the pollutants that have been detected in the discharge, and the receiving water's assimilative capacity. The assimilative capacity depends on the flow in the water receiving the discharge, and the concentration of the pollutant upstream. The greater the upstream flow, and the lower the upstream concentration, the greater the assimilative capacity is. Assimilative capacity may represent dilution (as in allocations for metals), or it may also incorporate the break-down of pollutants in the receiving water (as in allocations for oxygen-demanding materials).

The need for water-quality-based limits is determined by comparing the wasteload allocation for a pollutant to a measure of the effluent quality. The measure of effluent quality is called PEQ - Projected Effluent Quality. This is a statistical measure of the average and maximum effluent values for a pollutant. As with any statistical method, the more data that exists for a given pollutant, the more likely that PEQ will match the actual observed data. If there is a small data set for a given pollutant, the highest measured value is multiplied by a statistical factor to obtain a PEQ; for example if only one sample exists, the factor is 6.2, for two samples - 3.8, for three samples - 3.0. The factors continue to decline as samples sizes increase. These factors are intended to account for effluent variability, but if the pollutant concentrations are fairly constant, these factors may make PEQ appear larger than it would be shown to be if more sample results existed.

Summary of Permit Conditions

The draft limits and monitoring requirements for the Warren WPCC are very similar to the conditions in the current permit. Most effluent limits from the current permit would be carried over into the new permit.

Limits for selenium, and limits and monitoring for thallium, would be removed from the permit. Effluent data shows that these parameters no longer have the reasonable potential to contribute to exceedances of water quality standards.

New limits are included for free cyanide. The effluent data shows that cyanide discharges have the reasonable potential to exceed WQS. The permit contains a compliance schedule to allow the City to meet this new limit.

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Procedures for Participation in the Formulation of Final Determinations

The draft action shall be issued as a final action unless the Director revises the draft after consideration of the record of a public meeting or written comments, or upon disapproval by the Administrator of the U.S. Environmental Protection Agency.

Within thirty days of the date of the Public Notice, any person may request or petition for a public meeting for presentation of evidence, statements or opinions. The purpose of the public meeting is to obtain additional evidence. Statements concerning the issues raised by the party requesting the meeting are invited. Evidence may be presented by the applicant, the state, and other parties, and following presentation of such evidence other interested persons may present testimony of facts or statements of opinion.

Requests for public meetings shall be in writing and shall state the action of the Director objected to, the questions to be considered, and the reasons the action is contested. Such requests should be addressed to:

Legal Records Section
Ohio Environmental Protection Agency
P.O. Box 1049
Columbus, Ohio 43216-1049

Interested persons are invited to submit written comments upon the discharge permit. Comments should be submitted in person or by mail no later than 30 days after the date of this Public Notice. Deliver or mail all comments to:

Ohio Environmental Protection Agency Attention: Division of Surface Water Water Resource Management Section P.O. Box 1049 Columbus, Ohio 43216-1049

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Location of Discharge/Receiving Water Use Classification

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Recreation uses are defined by the depth of the waterbody and the potential for wading or swimming. Uses are defined for bathing waters, swimming/canoeing (Primary Contact) and wading only (Secondary Contact - generally waters too shallow for swimming or canoeing).

Water supply uses are defined by the actual or potential use of the waterbody. Public Water Supply designations apply near existing water intakes so that waters are safe to drink with standard treatment. Most other waters are designated for agricultural and industrial water supply.

The Lower Mahoning River study area is shown in Figure 2.

Facility Description

The Warren WPCC has a 16.0 MGD design flow and was last upgraded to advanced secondary treatment in February 1988. Treatment processes include grit removal, detritus setting tanks, extended aeration activated sludge, primary and final settling tanks, chlorination, and post aeration with the discharge to the mainstem at river mile (RM) 35.25. The sewage system is considered separate, but has had a history of problems with sanitary sewer overflows (SSOs) due to excessive inflow/infiltration (I/I).

Ten significant industrial users contribute approximately 3.4 MGD of flow to the treatment works. Eight of these industrial users are categorical industries (subject to U.S. EPA treatment technology regulations). The City of Warren has an approved pretreatment program to regulate these discharges.

Description of Existing Discharge

There is one outfall which is outfall 001.

Table 3 presents a summary of analytical results for outfall 001 effluent samples compiled from the annual pretreatment reports submitted by the City of Warren. The monthly average PEQ_{avg} and daily maximum PEQ_{max} decision criteria are also included on this table.

Table 4 presents a summary of unaltered monthly operation report data for the period January 1996 to June 2001 for the City of Warren as well as current permit limits, and monthly average PEQ_{avg} and daily maximum PEQ_{max} values.

Receiving Water Quality / Environmental Hazard Assessment

No current biological and chemical data exist to evaluate this discharge. Historical data (from 1994) show that this river segment did not meet the designated warmwater habitat aquatic life use. Ohio EPA believes that this non-attainment continues to exist, based on limited biological sampling from 2002 and 2003, along with historical chemical data on stream sediments and recent fish tissue chemistry.

The summary sheet from Ohio's 2006 Integrated Water Quality Monitoring and Assessment Report is attached to this fact sheet. The complete Integrated Report can be found on the Agency website at: http://www.epa.state.oh.us/dsw/tmdl/2006IntReport/2006OhioIntegratedReport.html.

Development of Water Quality-Based Limits

Determining appropriate effluent concentrations is a multiple step process in which parameters are identified as likely to be discharged by a facility, evaluated with respect to Ohio water quality criteria, and examined to determine the likelihood that the existing effluent could violate the calculated limits. In addition, antidegradation and whole effluent toxicity issues must be addressed.

As in past modeling studies, all facilities discharging to the Mahoning River mainstem between the Leavittsburg dam and the Ohio-Pennsylvania boundary are considered interactive and are included in the wasteload allocation (WLA). The WLA contains a total of 24 outfalls from 7 municipal WPCCs and 7 industrial facilities, as follows:

Warren Steel Holdings (CSC Industries) Thomas Steel Strip

Warren Consolidated Industries
Warren WPCC
Orion Power Midwest, Niles Plant
McDonald Steel
Youngstown WPCC
Struthers WPCC

ISG (Mittal) Steel
Reactive Metals Inc.
Niles WPCC
Girard WPCC
Campbell WPCC
Lowellville WPCC

Three dischargers located on tributaries are allocated separately from the mainstem discharges: Meander Creek WPCC (Meander Creek), Mosquito Creek WPCC (Mosquito Creek), and Boardman WPCC (Mill Creek). Travel time to and distance from the Mahoning River are considered large enough that, for modeling purposes, the effluents from the respective treatment plants are considered non-interactive with the direct dischargers to the Mahoning. Effluents from these three treatment plants were allocated to meet water quality standards for the conditions, habitat, and use designation for their particular receiving waters and separate Permit Support Documents were prepared for each facility. Monitoring was conducted at the mouths of these tributaries, however, for inputs into the Mahoning River mainstem model.

Parameter Selection

Effluent data for the Warren WPCC were used to determine what parameters should undergo wasteload allocation. The sources of effluent data are as follows:

Self-monitoring data (SWIMS)
Pretreatment program

January 2002 through December 2006 2003 through 2005

The effluent data were checked for outliers and the no values were eliminated from the data set. The average and maximum projected effluent quality (PEQ) values are presented in Table 5. For a summary of the screening results, refer to the parameter groupings at the end of this section.

Water Quality Standards

Ohio water quality standards (WQS) were used for all parameters except for chronic cadmium and chronic lead. The Mahoning River enters Pennsylvania at about river mile (RM) 11.43, and Pennsylvania WQS must be met at that point. Allocations for chronic cadmium and chronic lead were conducted to ensure that Pennsylvania WQS are met at the state line. The Pennsylvania Aquatic Life criteria and Human Health criteria were met at the state line for all other parameters (metals and organics).

Flows in the Mahoning River

Flows in the Mahoning River are contributed by a series of reservoirs in the headwaters and on Mosquito Creek, controlled and mostly owned by the U.S. Army Corps of Engineers. Constructed several decades ago to provide adequate flow for the steel industry of the Mahoning River valley, the reservoirs are operated on a schedule to maintain specific seasonal flows at Leavittsburg and Youngstown. The operation of the reservoir system is discussed at length in earlier USEPA Mahoning River studies (Amendola et al., 1977; Schregardus and Amendola, 1984).

Modeling Approach and Wasteload Allocations

Appropriate effluent concentrations for dischargers to the Mahoning River were determined using two models: a Monte Carlo model for the six commonly allocated metals (cadmium, chromium (total), copper, lead, nickel, and zinc) and the conventional Ohio EPA conservative parameter model (CONSWLA) for all other parameters. The models and their applications are discussed in the sections that follow and model inputs are presented.

Allocations are developed using a percentage of stream design flow (as specified in Table 7), and allocations cannot exceed the Inside Mixing Zone Maximum criteria. The data used in the WLAs are listed in Tables 6 and 7. The wasteload allocation results to maintain all applicable criteria are presented in Table 8. The current permit limits for NH₃-N were evaluated and found to be adequate to maintain the instream WQS for NH₃-N. Therefore, NH₃-N will not be addressed further in this report.

Dissolved Metals Translators

A dissolved metals translator (DMT) is the factor used to convert a dissolved metal aquatic life criterion to an effective total recoverable aquatic life criterion with which a total recoverable aquatic life allocation can be calculated as required in the NPDES permit process. Currently, a DMT is based on site- or area-specific field data; each field data sample consists of a total recoverable measurement paired with a dissolved metal measurement. For Mahoning River, there were 5 such paired samples available applicable to copper, lead, and silver. To account for the limited quantity of data, the DMT for each of these metals was determined as the lower end of the 95% confidence interval (1-tail) about the geometric mean of the total recoverable-to-dissolved ratios of the sample pairs. A DMT for zinc, cadmium, chromium, and nickel could not be determined due to shortcomings in the data. Each DMT is metal-specific and is applied by multiplying the dissolved criteria by the DMT, resulting in total effective recoverable criteria which can be used in the wasteload allocation procedures.

The Monte Carlo Model

The application of the Monte Carlo method was limited to the six commonly allocated metals (cadmium, chromium (total), copper, lead, nickel, and zinc). Previous allocations, using the conventional Ohio EPA conservative parameter model, resulted in stringent limits for these parameters that have been difficult for dischargers to maintain. As a result, the Ohio EPA was asked to consider other methods for determining effluent limits that would adequately protect the river while allowing the dischargers some relief. The Monte Carlo method addresses these concerns but does not guarantee more favorable discharge limits. This is the third permit cycle where a Monte Carlo method was used to determine the wasteload allocations for the six metals listed above.

Conventional water quality modeling methods project the receiving water pollutant concentration which will occur under critical low-flow conditions. The Monte Carlo probabilistic method, as applied to water quality modeling, projects the year-round probability distribution for the pollutant. This allows a more accurate determination of the frequency at which water quality criteria are violated or maintained. Conventional modeling methods, when applied to systems with numerous dischargers, may be overly conservative because they model all dischargers at their maximum permitted concentration. The more dischargers modeled, the more unlikely it is that all will discharge at their maximum level at the same time <u>and</u> at critical low-flow conditions. The Monte Carlo method accounts for the independent variability of discharges as well as other model inputs.

The Monte Carlo model for the Mahoning River was originally developed by Limno-Tech, Inc., for their 1993 study to determine alternative copper limits for Thomas Strip Steel. The model combines the Monte Carlo statistical method with a multi-discharge mass-balance model and allows upstream flow to be input from a historical gaging station flow record, in order to to account for unusual flow fluctuations caused by the numerous upstream dams and reservoirs. Ohio EPA approved the alternative limits developed using this model and received permission to modify and apply the model in the future. The original model was written in 1992-1993 in Borland Pascal. For this permit cycle, the model has been modified by the Ohio EPA and re-written in the 'C' programming language.

River Hardness and Water Quality Criteria

Water quality criteria for the six metals depends on instream hardness. Thus, hardness is a key element in determining effluent limits. A detailed analysis of the available hardness and flow data was conducted. This analysis revises and updates the Ohio EPA analysis previously performed in 2002. Stream hardness data was taken from the two main STORET stations on the Mahoning River main stem, at Leavittsburg, Ohio (RM 45.51) and at Lowellville, Ohio (RM 12.42). The hardness data for the two stations was analyzed for the period January 1997 to October 2006.

A linear correlation between the Leavittsburg USGS gaging station flow and instream hardness was determined for both STORET stations. These correlations were then used to calculate hardness as a function of river mile at 127 cfs (Leavittsburg 1Q10 low flow) and 135 cfs (7Q10 low flow).

Acute Criteria, at 1Q10river hardness (mg/L) = (-0.575)(river mile) + 184.534

Chronic Criteria, at 7Q10river hardness (mg/L) = (-0.575)(river mile) + 184.291

Discharger hardness was calculated with these equations. This relationship established local river hardness for calculating outside-mixing-zone, hardness-dependent criteria in the Monte Carlo model. Inside-mixing-zone, maximum criteria were determined with effluent hardness data when available, or outside-mixing-zone hardness when effluent data was unavailable.

Table 1 contains the water quality criteria for the six metals in the vicinity of the Warren WPCC.

This Monte Carlo method uses a thirty-day averaging period with a ten-year return period for meeting chronic (average) water quality criteria. A one-day averaging period with a ten-year return period is used for meeting the acute (maximum) water quality criteria. Since the chronic aquatic life criteria are less than or approximate to both the agriculture and human health criteria and since the return periods for both agriculture and human health criteria would be longer than ten years, the allocations that meet the average aquatic life criteria will be protective of the agriculture and human health criteria as well.

Federal rules require that a downstream state's water quality criteria be considered when calculating effluent limits. The Pennsylvania state line is at RM 11.43. Pennsylvania's standards are the same as Ohio's for copper, total chromium, nickel, and zinc. However, Pennsylvania's standards for cadmium and lead are more stringent than Ohio's and had to be considered. Since Pennsylvania uses, in effect, a one hundred-day return period, Ohio's acute criteria for those two metals, in combination with a ten-year return period, still meet Pennsylvania's water quality criteria. However, the same is not true for the chronic criteria.

Table 1. Water Quality Criteria for Monte Carlo Model Parameters (Warren WPCC)

		Outsi	Inside			
			verage		Maximum	Mixing
		Human	Agri-	Aquatic	Aquatic	Zone
Parameter (µg/L)	Health	culture ^A	Life ^B	Life ^B	Maximum	2
Cadmium		-	50.	0.41^{E}	7.9	19.
Chromium, total		-	100.	130.	2700.	6100.
Copper		1300.	500.	15. ^D	24. ^D	51.
Lead		-	100.	$6.1^{D,E}$	$240.^{D}$	550.
Nickel		610. ^E	200.	79.	710.	1600.
Zinc		69000.	25000.	180.	180.	410.

A There is some uncertainty regarding the return period used to develop the Agricultural Water Supply (AWS) criteria. Therefore, the AWS criteria for the Monte Carlo model are presented for information purposes only.

Data Analysis for the Monte Carlo Model

The Monte Carlo method accounts for individual system component variability by generating probability distributions that predict a range of possible input conditions. These distributions are derived from the mean and the coefficient of variation input by the user and based on field data for each of these components. Table 2 lists the calculated mean and coefficient of variation for such system characteristics as background/ambient concentrations and discharger and tributary flows.

Based on river hardness of 164 mg/L.

^C Based on effluent hardness of 189 mg/L.

D Effective Criteria Based on Application of Dissolved Metal Translator.

^E Pennsylvania WQC at the state line.

Table 2. Monte Carlo Model Inputs

	ent of Variation			
Parameter	Mean	Acute	Chronic	Source
Mahaning Divar at Laguittahung				
Mahoning River at Leavittsburg Flow (MGD) ^A				USGS
Cadmium (µg/L)	0.0	0.0	0.0	STORET
Chromium (µg/L) Chromium, total (µg/L)	0.0	0.0	0.0	STORET
Copper (µg/L)	0.0	0.0	0.0	STORET
Lead (µg/L)	1.242	0.739	0.135	STORET
Leau (μg/L) Nickel (μg/L)	0.0	0.739	0.133	STORET
Zinc (µg/L)	8.966	0.507	0.093	STORET
Zinc (µg/L)	8.900	0.307	0.093	SIUKEI
Mosquito Creek at mouth				
Flow (MGD)	80.65	1.44	0.263	USGS/SWIMS
Cadmium (µg/L)	0.0	0.0	0.0	STORET
Chromium, total (µg/L)	0.0	0.0	0.0	STORET
Copper (µg/L)	1.916	0.326	0.060	STORET
Lead (µg/L)	3.7	0.383	0.070	STORET
Nickel (µg/L)	0.0	0.0	0.0	STORET
Zinc (µg/L)	18.45	0.607	0.111	STORET
Meander Creek at mouth				
Flow (MGD)	3.706	0.330	0.060	SWIMS
Cadmium (µg/L)	0.0	0.550	0.000	STORET
Chromium, total (µg/L)	0.0	0.0	0.0	STORET
Copper (µg/L)	2.614	0.895	0.163	STORET
Copper (μg/L) Lead (μg/L)	1.509	1.192	0.103	STORET
Lead (μg/L) Nickel (μg/L)	0.0	0.0	0.218	STORET
Zinc (µg/L)	28.394	0.468	0.085	STORET
Zine (µg/L)	20.394	0.408	0.063	STOKET
Little Squaw Creek at mouth				
Flow (MGD)	2.808	0.537	0.098	SWIMS
Cadmium (µg/L)	0.095	2.425	0.443	SWIMS
Chromium, total (µg/L)	2.722	1.229	0.224	SWIMS
Copper (µg/L)	7.603	1.155	0.211	SWIMS
Lead (µg/L)	0.0	0.0	0.0	SWIMS
Nickel (µg/L)	2.644	2.621	0.479	SWIMS
Zinc (µg/L)	70.56	0.949	0.173	SWIMS

Table 2. Monte Carlo Model Inputs (continued)

		Coefficie	nt of Variation	
Parameter	Mean	Acute	Chronic	Source
Mill Creek at mouth				
Flow (MGD)	44.52	2.23	0.407	USGS
Cadmium (µg/L)	0.12	0.48	0.088	STORET
Chromium, total ($\mu g/L$)	0.0	0.0	0.0	STORET
Copper (µg/L)	2.37	0.70	0.127	STORET
Lead (µg/L)	4.12	1.95	0.356	STORET
Nickel (µg/L)	28.1	0.30	0.055	STORET
Zinc (µg/L)	13.5	1.87	0.34	STORET
Discharger flows (MGD)				
Warren Steel Holdings (CSC)	0.657	0.905	0.165	SWIMS
Thomas Steel Strip	1.11	0.336	0.061	SWIMS
Warren Consolidated Industrie	S			
003	0.094	0.528	0.096	SWIMS
006	0.002	0.340	0.062	SWIMS
007	2.48^{C}	0.314	0.057	SWIMS
008	6.50	0.179	0.033	SWIMS
Intake ^B				
013	38.25	0.188	0.034	SWIMS
010	0.442	0.473	0.086	SWIMS
011	0.601	0.346	0.063	SWIMS
012	0.158	0.184	0.034	SWIMS
Mittal 014	3.512	0.359	0.066	SWIMS
Warren WPCC 14.28	0.440	0.080	SWIMS	
Reactive Metals Inc.	0.374	0.408	0.075	SWIMS
Orion Power				
002	3.437	0.300	0.055	SWIMS
008	0.001	0.0	0.0	SWIMS
Niles WPCC	5.512	0.558	0.102	SWIMS
McDonald Steel	0.725	0.310	0.057	SWIMS
Youngstown WPCC	37.25	0.313	0.057	SWIMS
Campbell WPCC	1.624	0.515	0.094	SWIMS
Struthers WPCC	4.643	0.306	0.056	SWIMS
Lowellville WPCC	0.358	0.666	0.122	SWIMS

^A Each iteration of the model sequentially selects an upstream flow from the historical flow record at this

Intake flow was set equal to the sum of the WCI effluent flows plus the Mittal flow, multiplied by 0.871. (12.9% of the WCI / Mittal flow comes from sources other than the intake.)
 Recommended by Erm Gomes; outfall is submerged and no recent flows are available

The Conservative Substance Wasteload Allocation Model (CONSWLA) was used to allocate all parameters not included in the Monte Carlo model. CONSWLA is the model Ohio EPA typically uses in multiple discharger situations. Contrary to the Monte Carlo model, described above, CONSWLA model inputs for flow are fixed at their critical low levels and inputs for effluent flow are fixed at their design or 50th percentile levels. Background concentrations are fixed at a representative value (generally a 50th percentile). A mass balancing method is then used to allocate effluent concentrations that maintain WQS under these conditions. This technique is appropriate when data bases are unavailable to generate statistical distributions for inputs (like those used in the Monte Carlo method) and if the parameters modeled are conservative.

Reasonable Potential

After appropriate effluent limits are calculated (using the Monte Carlo and CONSWLA models), the reasonable potential of the discharger to violate the WLA (and the WQS) must be determined. Each parameter is examined and placed in a defined "group". Parameters that do not have a WQS or do not require a WLA based on the initial screening are assigned to either group 1 or 2. For the allocated parameters, the most restrictive average WLA and the maximum WLA were selected from Table 8. The average PEQ value (Table 5) is compared to the average PEL, and the maximum PEQ value is compared to the maximum PEL. Based on the calculated percentage of the respective average and maximum comparisons, the parameters are assigned to "groups", as listed in Table 9.

Whole Effluent Toxicity WLA

Whole effluent toxicity or "WET" is the total toxic effect of an effluent on aquatic life measured directly with a toxicity test. Acute WET measures short term effects of the effluent while chronic WET measures longer term and potentially more subtle effects of the effluent.

Water Quality Standards for WET are expressed in Ohio's narrative "free from" WQS rule (OAC 3745-1-04(D)). These "free froms" are translated into toxicity units (TUs) by the associated WQS Implementation Rule (OAC 3745-2-09). Wasteload allocations can then be calculated using TUs as if they were water quality criteria.

The wasteload allocation calculations for WET are similar to those for aquatic life criteria (using the chronic toxicity unit (TU_c) and 7Q10 for average and the acute toxicity unit (TU_a) and 1Q10 for maximum). An assessment of the biological and hydraulic data in the vicinity of the Warren WPCC indicated that the effluent acute toxicity is interactive with ISG Mittal Steel and the Warren Consolidated Industries discharges. For the Warren WPCC, the AET values are $0.48\ TU_a$ and $7.01\ TU_c$.

The chronic toxicity unit (TU_c) is defined as 100 divided by the IC₂₅:

$$TU_{c} = \underline{100}_{IC_{25}}$$

This equation applies outside the mixing zone for warmwater, modified warmwater, exceptional warmwater, coldwater, and seasonal salmonid use designations except when the following equation is more restrictive (Ceriodaphnia dubia only):

The acute toxicity unit (TU_a) is defined as 100 divided by the LC50 for the most sensitive test species:

$$TU_a = 100$$

This equation applies outside the mixing zone for warmwater, modified warmwater, exceptional warmwater, coldwater, and seasonal salmonid use designations.

When the calculated wasteload allocation is less than 1.0 TU_a, the wasteload allocation is defined as:

Dilution Ratio	Allowable Effluent Toxicity
(downstream flow to discharger flow)	(percent effects in 100% effluent)
	_
up to 2 to 1	30
greater than 2 to 1 but less than 2.7 to 1	40
2.7 to 1 to 3.3 to 1	50

The WLA is 40% mortality in 100% effluent based on the dilution ratio of 2.4 to 1 (based on discharges from the three permittees used in the WET allocation.

Effluent Limits/Hazard Management Decisions

After appropriate effluent limits are calculated, the reasonable potential of the discharger to violate the WLA (and the WQS) must be determined. Each parameter is examined and placed in a defined "group". Parameters that do not have a WQS or do not require a WLA based on the initial screening are assigned to either group 1 or 2. For the allocated parameters, the Preliminary Effluent Limit (PEL) for the most restrictive average and maximum WLA were selected from Table 9. The PEL_{avg} was compared to the PEQ_{avg} value from Table 5, and the PEL_{max} was compared to the PEQ_{max} value. Based on the calculated percentage of the allocated value, the parameters are assigned to group 3, 4 or 5. The listing in Table 9 (Parameter Assessment Table) reflects the hazard assessment done according to WLA procedures. Table 10 (Final Effluent Limits Table) shows the draft NPDES limits for the City of Warren.

Limits proposed for oil and grease, pH, fecal coliform, and dissolved oxygen are based on Water Quality Standards (OAC 3745-1).

Proposed limits for total suspended solids (TSS), ammonia-nitrogen (NH₃-N), 5-day carbonaceous biochemical oxygen demand (CBOD₅), and dissolved oxygen (D.O.) are all based on plant design.

The Ohio EPA risk assessment (Table 10) places free cyanide in group 5. This placement as well as the data in Tables 3, 4, and 5 indicate that the reasonable potential to exceed water quality standards exists and limits are necessary to protect water quality. The thirty day average limit and the daily maximum limits are based on Wasteload Allocation (WLA).

The limit for residual chlorine would be continued in the new permit because it is one of the basic operating parameters for the plant. The draft limit is based on the current permit limit because it is slightly more restrictive than the new wasteload allocation. State and federal antibacksliding rules require the use of the current limit in this situation [see OAC 3745-33-05(E) and 40 CFR 122.45].

Ohio EPA risk assessment (Table 9) places cadmium, mercury and selenium in group 4. This placement as well as the data in Tables 3, 4, and 5 support that these parameters should not pose an environmental hazard and limits are not necessary to protect water quality. Monitoring is proposed to document that these pollutants continue to remain at low levels.

For mercury, the permit contains an additional requirement for the next permit application. This condition requires the City to assess compliance with the monthly average water quality standard, and to submit a mercury variance request with the application if this concentration can not be achieved (see Part II, Item).

Ohio EPA risk assessment (Table 10) places chromium, hexavalent chromium, copper, lead, nickel, nitrate/nitrite and zinc in groups 2/3. This placement as well as the data in Tables 3, 4 and 5 support that these parameters should not pose an environmental hazard and limits are not necessary to protect water quality. Monitoring at a reduced frequency is proposed to document that these pollutants continue to remain at low levels.

Additional monitoring requirements proposed at the final effluent, influent, upstream/downstream and sludge stations are included for all facilities in Ohio and vary according to the type and size of the discharge. In addition to permit compliance, this data is used to assist in the evaluation of effluent quality and treatment plant performance and for designing plant improvements and conducting future stream studies

The Ohio 305 (b) Report indicates that nutrients are one of the causes of impairment to the Mahoning River so the following nutrients will be monitored: Phosphorus, Total Kjeldahl Nitrogen, and Nitrate+Nitrite-N.

The permit also contains a compliance schedule item to investigate and fix sources of excessive I/I in the sewer system. This condition is needed to prevent SSOs in the sewer network.

Whole Effluent Toxicity Reasonable Potential

WET values are compared to wasteload allocation values. This comparison along with an assessment of the instream community are two ways in which whole effluent toxicity is evaluated. For the Warren WPCC, the WLA values are 0.48 TU_a and 7.01 TU_c.

The Warren WPCC does not have the reasonable potential to exceed narrative water quality standards for toxicity. None of the four available test results showed acute or chronic toxicity to test organisms (see Table 4 for results).

The draft permit contains an annual chronic toxicity test requirements, with acute endpoints reported. U.S. EPA has informed Ohio EPA that state application requirements for publicly owned treatment works do not conform to federal rules because they do not require the submission of at least four toxicity tests. To address this requirement, Ohio EPA has begun to include annual testing in permits for major POTWs. Chronic tests are being included for Warren WPCC because the chronic WLA of 7.01 is less than the maximum acute chronic ratio usually seen in toxicity testing (20:1).

Table 3. Effluent Characterization and Decision Criteria

Summary of analytical results for Warren WPCC outfall 3PE00008001. All values are in μ g/l unless otherwise indicated. PT = data from, pretreatment program reports; OEPA = data from analyses by Ohio EPA; ND = below detection (detection limit); NA = not analyzed. Decision Criteria: PEQ_{avg} = monthly averages; PEQ_{max} = daily maximum analytical results.

	PT	PT	PT	PT	DECISIO	N CRITERIA
PARAMETER	11/18/03	11/17/04	11/16/05	11/15/06	PEQ_{avg}	PEQ_{max}
Antimony	<10	<10	<10	10	24	33
Mercury	0.2	0.7	< 0.2	< 0.2	0.0085	0.0126
Nickel	<10	<10	16	<10	17	25
Selenium	18	13	<10	<10	17.5	24
Zinc	27	23	37	14	25	32
Cyanide, T.	70	70	60	50		

Table 4. Effluent Characterization and Decision Criteria

Summary of current permit limits and unaltered monthly operating report (MOR) data for the Warren WPCC outfall 001. All values are based on annual records unless otherwise indicated. N = Number of Analyses. * = For pH, 5th percentile shown in place of 50th percentile; ** = For dissolved oxygen, 5th percentile shown in place of 95th percentile; A = 7 day average. Decision Criteria: $PEQ_{avg} = monthly$ average; $PEQ_{max} = daily$ maximum analytical results.

			Current P	ermit Limits		Pe	ercentiles			Decision (Criteria
Parameter	Season	Units	30 day	Daily	# Obs.	50 th	95 th	Data Range	# Obs.	PEQ _{ave}	PEQ _{max}
Outfall 001											
Water Temperature	Annual	C	Mo	nitor	1826	16	20	10-22			
Dissolved Oxygen	Summer	mg/l	5.0 min.		878	7.6	10	5-11.6			
Dissolved Oxygen	Winter	mg/l	5.0 min.		870	7.9	11.2	5-12.8			
Chemical Oxygen Demand	Annual	mg/l	Mo	onitor	137	27	52.2	0-75			
(Low Level)											
pH, Maximum	Annual	S.U.		9.0	212	7	7.2	6.8-7.5			
pH, Maximum	Annual	S.U.		9.0	1614	7.3	7.8	6.6-8.4			
pH, Minimum	Annual	S.U.		6.5	212	6.9	7.1	6.5-7.5			
pH, Minimum	Annual	S.U.		6.5	1613	7.2	7.6	6.5-8.2			
Total Suspended Solids	Annual	mg/l	20	30^{A}	1242	3	13	1-48			
Oil and Grease, Total	Annual	mg/l		10	228	0.6	1.5	0-4.3			
Oil and Grease, Freon Extr-Grav	Annual	mg/l			30	0.85	2.29	0-2.9			
Method											
Nitrogen, Ammonia (NH3)	Summer	mg/l	3.0	4.5 ^A	634	0.37	2.2	0-5.5	424	2.41	3.30
Nitrogen, Ammonia (NH3)	Winter	mg/l	15	22^{A}	609	0.52	7.72	0-12	302	6.13	8.40
Nitrogen Kjeldahl, Total	Annual	mg/l	Mo	nitor	239	4	10.5	0.62-15.4			
Nitrite Plus Nitrate, Total	Annual	mg/l		nitor	245	8.7	13.5	0.91-16.4	245	8.38	11.48
Phosphorus, Total (P)	Annual	mg/l		nitor	230	0.675	1.23	0.14-2.1	230	1.05	1.43
Cyanide, Free	Annual	mg/l		nitor	120	0	0.0205	0-0.06	136	0.022	0.024
Cyanide, Free	Annual	mg/l		nitor	16	0	0.0125	0-0.014	136	0.022	0.024
Selenium, Total Recoverable	Annual	ug/l	26		123	7.6	23	0-30	123	17.5	24
Thallium, Total Recoverable	Annual	ug/l	4.3	160	2	0	0	0-0	123	2.3	3.2
Thallium, Total (TL)	Annual	ug/l	4.3	160	121	0	0	0-4	123	2.3	3.2
Nickel, Total Recoverable	Annual	ug/l		nitor	16	0	14.3	0-21	136	17	25
Nickel, Total Recoverable	Annual	ug/l		nitor	120	0	21.1	0-61	136	17	25
Zinc, Total Recoverable	Annual	ug/l	Mo	nitor	137	17	29	9-42	137	25	32

			Current Permit Limits			Per	rcentiles			Decision Criteria	
Parameter	Season	Units	30 day	Daily	# Obs.	50 th	95 th	Data Range	# Obs.	PEQ _{ave}	PEQ _{max}
Outfall 001											
Antimony, Total Recoverable	Annual	ug/l	Mo	nitor	2	0	0	0-0	54	24	33
Antimony, Total	Annual	ug/l	Mo	nitor	52	0	21	0-45	54	24	33
Cadmium, Total Recoverable	Annual	ug/l	Mo	nitor	16	0.75	1.5	0-1.5	137	1.4	2.1
Cadmium, Total Recoverable	Annual	ug/l	Mo	nitor	121	0.5	1.5	0-3	137	1.4	2.1
Lead, Total Recoverable	Annual	ug/l	Mo	nitor	16	0	2.9	0-2.9	135	7.0	9.6
Lead, Total Recoverable	Annual	ug/l	Mo	nitor	119	0	0	0-12	135	7.0	9.6
Chromium, Total Recoverable	Annual	ug/l	Mo	nitor	138	0	0	0-7	138	4.1	5.6
Copper, Total Recoverable	Annual	ug/l	Mo	nitor	16	0	0	0-0	138	6.8	10
Copper, Total Recoverable	Annual	ug/l	Mo	nitor	122	0	10	0-14	138	6.8	10
Chromium, Dissolved Hexavalent	Annual	ug/l	Mo	nitor	71	0	1	0-3	71	2.2	3
Fecal Coliform	Annual	#/100 ml	1000	2000^{A}	405	80	1040	1-2100			
Bis(2-ethylhexyl) Phthalate	Annual	ug/l			2	0	0	0-0			
Flow Rate	Annual	MGD	Mo	nitor	1826	12.9	26.7	3.9-53.4			
Chlorine, Total Residual	Annual	mg/l		0.028	592	0.02	0.03	0-0.03	592	0.013	0.018
Mercury, Total	Annual	ug/l			16	0	0	0-0			
Mercury, Total (Low Level)	Annual	ng/l	Mo	nitor	53	4.24	9.74	0-27.7	53	8.5	12.6
Acute Toxicity, Ceriodaphnia dubia	Annual	TUa	Mo	nitor	4	0	0	0-0			
Chronic Toxicity, Ceriodaphnia dubia	Annual	TUc	Mo	nitor	4	0	0	0-0			
Acute Toxicity, Pimephales promelas	Annual	TUa	Mo	nitor	4	0	0.17	0-0.2			
Chronic Toxicity, Pimephales	Annual	TUc	Mo	nitor	4	0	0	0-0			
promelas											
CBOD 5 day	Summer	mg/l	12	18 ^A	636	3	6	1-10			
CBOD 5 day	Winter	mg/l	12	18 ^A	610	3	7	1-12			

^{*** - 7} day concentration

Table 5. Effluent Data for Warren WPCC

Parameter	Units		# of Samples	#> MDL	Average PEQ	Maximum PEQ
Self-Monitoring (SWIMS) Da	<u>ata</u>					
Ammonia	mg/L	Summer	424	354	2.409	3.30
Ammonia	mg/L	Winter	302	281	6.132	8.40
Nitrate+Nitrite	mg/L		245	245	8.38	11.48
Phosphorus	mg/L		230	230	1.052	1.429
Cyanide, free	μg/L		136	22	22.49	23.855
Selenium	μg/L		123	64	17.52	24.0
Thallium	μg/L		123	1	2.336	3.2
Nickel	μg/L		136	52	16.982	24.988
Zinc	μg/L		137	137	24.787	31.644
Antimony	μg/L		54	5	23.567	32.896
Cadmium	μg/L		137	72	1.411	2.144
Lead	μg/L		135	8	7.01	9.6
Chromium, tot.	μg/L		138	1	4.088	5.6
Copper	μg/L		138	13	6.753	10.089
Chromium +6, diss.	μg/L		71	4	2.19	3.0
Bis(2-ethylhexyl)phthalate ^A	μg/L		2	0		
TRC	μg/L		592	321	13.14	18.0
Mercury	μg/L		53	51	0.0085	0.0126
Pretreament Program						
Cyanide, total	μg/L		3	3	0.153	0.21

^A Carcinogen

Table 6. Water Quality Criteria Used in the CONSWLA Model

Table 6. Water Quarty Cite	eria Osea ili tile	Outside Mixing Zone Criteria							
				_	Inside				
			Average		Maximum	_			
		Human	Agri-	Aquatic	Aquatic	Zone			
Parameter	Units	Health	culture	Life	Life	Maximum			
Antimony	μg/L	14. ^C	_	190.	900.	1800.			
Arsenic	μg/L	50. ^C	100.	150.	340.	680.			
Bis(2-Ethylhexl)Phthalate	μg/L	1.8 ^C	_	8.4	1100.	2100.			
Barium	μg/L	2400. ^C	_	220.	2000.	4000.			
Boron	μg/L	3100. ^C	_	950.	8500.	17000.			
Bromomethane	μg/L	48. ^C	_	16.	38.	75.			
Bromodichloromethane	μg/L	460.	_	_	_	_			
Butylbenzyl phthalate	μg/L	300. ^C	_	23.	130.	260.			
Chlorine, tot. res.	μg/L	_	_	11.	19.	38.			
Chloroform	μg/L	5.7 ^C	_	140.	1300.	2600.			
Chromium +6, diss.	μg/L	_	_	10. ^C	16.	31.			
Cobalt	μg/L	_	_	24.	220.	440.			
Cyanide, free	mg/L	700. ^c	_	5.2 ^C	22. ^C	92.			
1,4-Dichlorobenzene	μg/L	2600.	_	9.4	57.	110.			
Dichloromethane	μg/L	16000.	_	1900.	11000.	22000.			
Di-n-butyl phthalate	μg/L	2700. ^C	_	21. ^C	110. ^C	_			
Fluoride	μg/L	_	2000.	_	_	_			
Iron	μg/L	_	5000.	_	_	_			
Mercury A	μg/L	0.012	10.	0.91	1.7	3.4			
Molybdenum	μg/L	_	_	20000.	190000.	370000.			
Naphthalene	μg/L	_	_	21.	170.	340.			
Nitrate+Nitrite	mg/L	_	100.	_	_	_			
Phenol	μg/L	21000. ^c	_	400.	4700.	9400.			

A Bioaccumulative Chemical of Concern (BCC)
 C Pennsylvania Water Quality Criteria.

Table 6. Water Quality Criteria in the Study Area - Continued.

		0	Outside Mixing Zone Criteria							
						Inside				
			Average		Maximun	n Mixing				
		Human	Agri-	Aquatic	Aquatic	Zone				
Parameter	Units	Health	culture	Life	Life	Maximum				
Selenium	μg/L	11000.	50.	5.0	_	_				
Silver (Seg. 1)	μg/L μg/L	_	-	1.3	9.4^{E}	51. ^E ,F				
Silver (Seg. 2)	μg/L	_	_	1.3	$25^{\rm E,F}$	$75.^{\mathrm{E}}$,F				
Silver (Seg. 3)	μg/L	_	_	1.3	$23.^{E,F}$	110. ^E ,F				
Silver (Seg. 4)	μg/L	_	_	1.3	22. ^E ,F	55. ^E ,F				
Silver (Seg. 6)	μg/L	_	_	1.3	22. ^E ,F	37. ^E ,F				
Silver (Seg. 9)	μg/L	_	_	1.3	$23.^{\mathrm{E}}$,F	51. ^E ,F				
Strontium	μg/L	_	_	5300.	48000.	95000.				
Thallium	μg/L	1.7 ^C	_	13. ^c	65. ^C	160.				
Total Dissolved Solids	mg/L	_	_	1500.	_	_				
Toluene	μg/L	6800. ^C	_	62.	560.	1100.				

^C Pennsylvania Water Quality Criteria.

Table 7. Instream Conditions and Discharger Flow for CONSWLA Model

E Local river hardness at critical low design flow was used to determine the water quality criteria. Segment 1 is at the Ohio Pennsylania state line (RM 11.43, hardness = 179 mg/L), Segment 2 is from the Orion Power Intake to the Ohio Pennsylania state line (RM 29.7 - RM11.43, hardness - 177 mg/L), Segment 3 is the WCI Intake to the Orion Power Intake (RM 36.5 to Rm 29.7, hardness = 168 mg/L), Segment 4 is from Leavittsburg to the WCI Intake (RM 45.5 to RM 36.5, hardness = 165 mg/L), Segment 6 is an unnamed tributary to the Mahoning that Mittal discharges to (hardness = 165 mg/L), and Segment 9 is Little Squaw Creek (hardness = 171 mg/L).

^F Effective Criteria Based on Application of Dissolved Metal Translator.

Parameter	Units/Outf	all	Value	Basis
Mahoning River Upstrea	am			
7Q10	cfs	annual	135	USGS gage #03094000, 1969-06 data
1Q10	cfs	annual	127	USGS gage #03094000, 1969-06 data
30Q10	cfs	summer	178	USGS gage #03094000, 1969-06 data
	cfs	winter	191	USGS gage #03094000, 1969-06 data
HMQ	cfs	annual	379	USGS gage #03094000, 1969-06 data
Meander Creek at mouth	1			
7Q10	cfs	annual	6.19	USGS gage #03097500, 1929-51 data
1Q10	cfs	annual	6.19	USGS gage #03097500, 1929-51 data
30Q10	cfs	summer	6.19	USGS gage #03097500, 1929-51 data
	cfs	winter	6.19	USGS gage #03097500, 1929-51 data
HMQ	cfs	annual	6.19	USGS gage #03097500, 1929-51 data
Mosquito Creek at mout	h			
7Q10	cfs	annual	10.6	USGS gage #03095500, 1954-91 data
1Q10	cfs	annual	9.47	USGS gage #03095500, 1954-91 data
30Q10	cfs	summer	14.0	USGS gage #03095500, 1954-91 data
_	cfs	winter	12.6	USGS gage #03095500, 1954-91 data
HMQ	cfs	annual	28.0	USGS gage #03095500, 1954-91 data
Mill Creek at mouth				
7Q10	cfs	annual	9.99	USGS gage #03098500, 1952-71 data
1Q10	cfs	annual	9.87	USGS gage #03098500, 1952-71 data
30Q10	cfs	summer	10.7	USGS gage #03098500, 1952-71 data
	cfs	winter	15.7	USGS gage #03098500, 1952-71 data
HMQ	cfs	annual	14.3	USGS gage #03098500, 1952-71 data
Discharger Flow	cfs			
CSC Industries	005		2.17	NEDO
Thomas Steel Strip	001		2.79	NEDO
Warren Consolidate			3.84	NEDO
Industries	008		9.78	NEDO
	010		0.71	NEDO
	011		0.99	NEDO
	012		0.248	NEDO
	013		53.38	NEDO
	015		1.72	NEDO
	016		1.81	NEDO
ISG Steel	014		7.27	NEDO
Warren WPCC	001		24.8	NEDO
Reactive Metals, Inc			0.696	NEDO
Niles WPCC	001		9.59	NEDO
McDonald Steel	001		1.45	NEDO

Table 7. Instream Conditions and Discharger Flow for CONSWLA Model - Continued.

	Jnits/Outfa	all	Value	Basis
Discharger Flow	cfs			
Magazita Casalt WDC	7 001		6.5	NEDO
Mosquito Creek WPC			6.5	NEDO NEDO
Meander Creek WPCC			6.19	NEDO
Boardman WPCC	001		7.74	NEDO
Orion Power	001		298.6	NEDO
	002		6.19	NEDO
	008		0.002	NEDO
Girard WPCC	001		7.74	NEDO
Youngstown WPCC	001		54.2	NEDO
Campbell WPCC	001		2.94	NEDO
Struthers WPCC	001		9.28	NEDO
Lowellville WPCC	001		0.792	NEDO
Mixing Assumption	%	average	100	Stream-to-discharge ratio
8	%	maximum	100	Stream-to-discharge ratio
				and the second s
Instream Temperature	°C	summer	22	STORET ^C ; 38 values, 0 <mdl, 1990-98<="" td=""></mdl,>
		winter	4.1	STORET ^C ; 27 values, 0 <mdl, 1990-98<="" td=""></mdl,>
		***************************************		5101E1 , 27 (alaes, 6 4)15E, 1996 96
Instream pH	S.U.	summer	7.8	STORET ^c ; 38 values, 0 <mdl, 1990-98<="" td=""></mdl,>
mstream pri	5.0.	winter	7.9	STORET ^c ; 27 values, 0 <mdl, 1990-98<="" td=""></mdl,>
		WIIICI	1.5	STORET , 27 values, 6 dilbe, 1996 96
Background Water Quality	,			
Ammonia	mg/L	summer	0.09	STORET; 42 values, 8 <mdl, 1999-2005<="" td=""></mdl,>
7 Hillionia	mg/L	winter	0.13	STORET; 16 values, 0 <mdl, 1999-2005<="" td=""></mdl,>
Arsenic	μg/L	annual	2.0	STORET; 124 values, 54 <mdl, 1999-2005<="" td=""></mdl,>
Antimony	μg/L μg/L	annual	0.0	No representative data available
Barium	μg/L μg/L	annual	36.	STORET; 124 values, 0 <mdl, 1999-2005<="" td=""></mdl,>
Boron	μg/L μg/L	annual	0.	No representative data available
			0.	No representative data available
Bis(2E)Phthalate	μg/L	annual annual		•
Butylbenzyl phthalate	μg/L		0.	No representative data available
Cadmium	μg/L	annual	0.	STORET ^c ; 82 values, 82 <mdl, 1999-2006<="" td=""></mdl,>
Chlorine, total res	μg/L	annual	0.	No representative data available
Chromium, tot.	μg/L	annual	0.	STORET ^c ; 82 values, 81 <mdl, 1999-2006<="" td=""></mdl,>
Chromium ⁺⁶ , diss	μg/L	annual	0.	No representative data available
Chloroform	μg/L	annual	0.	No representative data available
Copper	μg/L	annual	0.	STORET ^C ; 82 values, 81 <mdl, 1999-2006<="" td=""></mdl,>
Cyanide free	μg/L	annual	0.	No representative data available
Fluoride	μg/L	annual	0.	No representative data available
Iron	μg/L	annual	747.	STORET; 124 values, 0 <mdl, 1999-2005<="" td=""></mdl,>
Lead	μg/L	annual	1.24	STORET ^c ; 82 values, 70 <mdl, 1999-2006<="" td=""></mdl,>
Mercury	μg/L	annual	0.	No representative data available
Molybdenum	μg/L	annual	0.	No representative data available

Table 7. Instream Conditions and Discharger Flow for CONSWLA Model - Continued

Parameter	Units/C	Outfall	Value	Basis
Background Water Qual	ity (Cont.)			
	~			
Naphthalene	μg/L	annual	0.	No representative data available
Nickel	μg/L	annual	0.	STORET ^C ; 82 values, 82 <mdl, 1999-2006<="" td=""></mdl,>
Phenol	μg/L	annual	0.	No representative data available
Selenium	μg/L	annual	0.	STORET; 15 values, 15 <mdl,< td=""></mdl,<>
Silver	μg/L	annual	0.	No representative data available
Strontium	μg/L	annual	151.	STORET; 124 values, 0 <mdl, 1999-2005<="" td=""></mdl,>
Thallium	μg/L	annual	0.	No representative data available
Toluene	μg/L	annual	0.	No representative data available
TDS	mg/L	annual	307.	STORET; 109 values, 0 <mdl, 1999-2005<="" td=""></mdl,>
Zinc	μg/L	annual	8.97	STORET ^c ; 82 values, 55 <mdl, 1999-2006<="" td=""></mdl,>

^C STORET station # 602280 Mahoning River @ Leavittsburg - Leavitt Rd. RM 45.51

Table 8. Summary of Effluent Limits to Maintain Applicable Water Quality Criteria

		<i>E</i>	Average		Maximum	Inside
		Human	Agri	Aquatic	Aquatic	Mixing Zone
Parameter	Units	Health	Supply	Life	Life	Maximum
Antimony ^B	μg/L	684. ^E	_	977.	4435. ^A	1800.
Arsenic ^B	μg/L	811. ^{AE}	1653. ^A	1040. ^A	2263. ^A	680.
Cadmium	μg/L			2.3 ^E	19. ^A	19.
Chlorine, total res summer	μg/L	_	_	16.	28.	38.
Chromium, tot. ^B	μg/L			688.	6100. ^A	6100.
Chromium ⁺⁶ , dissolved ^B	μg/L	_	_	60. ^{A E}	83. ^A	31.
Copper	μg/L			40. ^D	50. ^D	51.
Cyanide free	μg/L	700. ^{A E}	_	24. ^E	86. ^E	92.
Lead	μg/L			19. ^{D, E}	354. ^D	550.
Mercury ^C	μg/L	0.049	41. ^A	1.6	2.9	3.4
Molybdenum ^B	μg/L			140200.	1271000. ^A	370000.
Nickel ^B	μg/L			406.	1600. ^A	1600.
Selenium	μg/L	119000.	541.	24.	_	_
Silver ^B	μg/L			5.5	92. ^A	55.
Thallium	μg/L	84. ^E		102. ^E	453. ^{A E}	160.
Zinc ^B	μg/L			410.	346.	410.

Allocation must not exceed the Inside Mixing Zone Maximum.

Parameter would not require a WLA based on reasonable potential procedures, but allocation requested for use in pretreatment program.

Bioaccumulative Chemical of Concern (BCC); no mixing zone allowed after 11/15/2010, WQS must be met at end-of-pipe - unless the requirements for an exception are met as listed in 3745-2-08.

^D WLA based on applicable dissolved metal translator.

E Pennsylvania water quality criteria was applied

<u>Group 1</u>: Due to a lack of criteria, the following parameters could not be evaluated at this time.

Cyanide, total Phosphorus

Group 2: PEQ < 25% of WQS or all data below minimum detection limit; WLA not required. No

limit recommended, monitoring optional.

Antimony Arsenic Bis(2-Ethylhexl)Phthalate

Chromium⁺⁶, diss. Chromium, tot. Molybdenum

Nickel Nitrate+Nitrite-N Silver

Zinc

<u>Group 3</u>: $PEQ_{max} < 50\%$ of maximum PEL and $PEQ_{avg} < 50\%$ of average PEL. No limit

recommended, monitoring optional.

Copper Mercury (<11/15/2010) Lead

Thallium

Group 4: PEQ_{max} \geq 50% but <100% of the maximum PEL or PEQ_{avg} \geq 50% but < 100% of the

average PEL. Monitoring is appropriate.

Cadmium Chlorine, total res Mercury (>11/15/2010)

Selenium

Group 5: Maximum PEQ \geq 100% of the maximum PEL or average PEQ \geq 100% of the average

PEL, or either the average or maximum PEQ is between 75 and 100% of the PEL and

certain conditions that increase the risk to the environment are present. Limit recommended.

Limits to Protect Numeric Water Quality Criteria

		Applicable _	Recommended Effluent Limits		
Parameter	Units	Period	Average	Maximum	
Cyanide, free	μg/L	annual	24.	86.	

Table 10. Final effluent limits and monitoring requirements for the Warren WPCC outfall **3PE00008001** and the basis for their recommendation.

			Effluent Limits				
		Concentra		Loading (•		
		30 Day	Daily	30 Day	Daily	_	
Parameter	Units	Average	Maximum	Average	Maximum	Basis ^b	
Water Temperature	°C		Monito	r		\mathbf{M}^{c}	
Suspended Solids	mg/l	20	30^{d}	1211	1817	PD\EP	
Oil and Grease	mg/l		10			WQS	
Ammonia-N	mg/l					-	
Summer		3.0	4.5 ^d	182	273	WLA\EP\PD	
Winter		15	22^{d}	908	1332	WLA\EP\PD	
Fecal Coliform	#/100ml						
(Summer only)		1000	2000^{d}	_	_	WQS	
Flow	MGD		Monito	r		M ^c	
CBOD₅	mg/l	12	18 ^d	727	1090	PD\EP	
рH	S.U.		6.5 to	9.0		WQS	
Chlorine Residual	mg/l		0.028			ABS/EP	
Dissolved Oxygen	mg/l	n	ot less than 5.0	0		WQS\PD	
Phosphorus	mg/l		Monito	r		M ^c	
Nitrogen, Total	_						
Kjeldahl	mg/l		Monito	r		M ^c	
Selenium, T. R.	ug/l		Monito	r		M/RP°	
Zinc, T. R.	μg/l		Monito			M	
Chromium, T. R.	μg/l		Monito	r		M ^c	
Hex. Chromium	. •						
(Dissolved)	μg/l		Monito	r		M ^c	
Nickel, T. R.	μg/l		Monito	r		M ^c	
Lead, T. R.	μg/l		Monito	r		M ^c	
Copper, T. R.	μg/l		Monito			$\mathbf{M}^{\mathbf{c}}$	
Cadmium, T. R.	μg/l		Monito	r		M/RP ^c	
Mercury, T.	ng/l		Monito	r		M/RP°	
Cyanide, Free	mg/l	0.024	0.086	1.45	5.21	WLA	
NO2+NO3-N	mg/l		Monito	r		M ^c	
COD	mg/l		Monito			M ^c	
Whole Effluent	C						
Toxicity							
Acute	TUa		- Monitor (w/c	trigger)		M ^c	
Chronic	TUc		- Monitor (w/o			M ^c	

- ^a Any effluent loading limits for the following parameters are calculated using the Monte Carlo flow: Cadmium, Chromium (total), Copper, Lead, Nickel, and Zinc, and all the other parameters that need effluent loading limits are calculated using the CONSWLA flow. This is because of OAC 3745-33-07 (C) (1)(b). For this particular fact sheet the CONSWLA flow (of 24.8 (cfs) or 16.0 (MGD)) was used to calculate the effluent loading limitations of the Suspended Solids, Ammonia-N (summer), Ammonia-N (winter), CBOD₅, Chlorine residual, Cyanide, Selenium and Thallium.
- b Definitions:
- ABS = Antibacksliding Rule (OAC 3745-33-05(E) and 40 CFR Part 122.44(I)); AD = Antidegradation (OAC 3745-1-05); BPJ = Best Professional Judgment; BPT = Best Practicable Waste Treatment Technology, 40 CFR Part 133, Secondary Treatment Regulation; EP = Existing Permit; M = Monitoring; PD = Plant Design Criteria; RP = Reasonable Potential for requiring water quality-based effluent limits and monitoring requirements in NPDES permits (3745-33-07(A)); WET = Whole Effluent Toxicity (OAC 3745-33-07(B)); WLA = Wasteload Allocation procedures (OAC 3745-2); WLA/IMZM = Wasteload Allocation limited by Inside Mixing Zone Maximum; WQS = Ohio Water Quality Standards (OAC 3745-1).
- Monitoring of flow and other indicator parameters is specified to assist in the evaluation of effluent quality and treatment plant performance.
- ^d 7 day average limit.

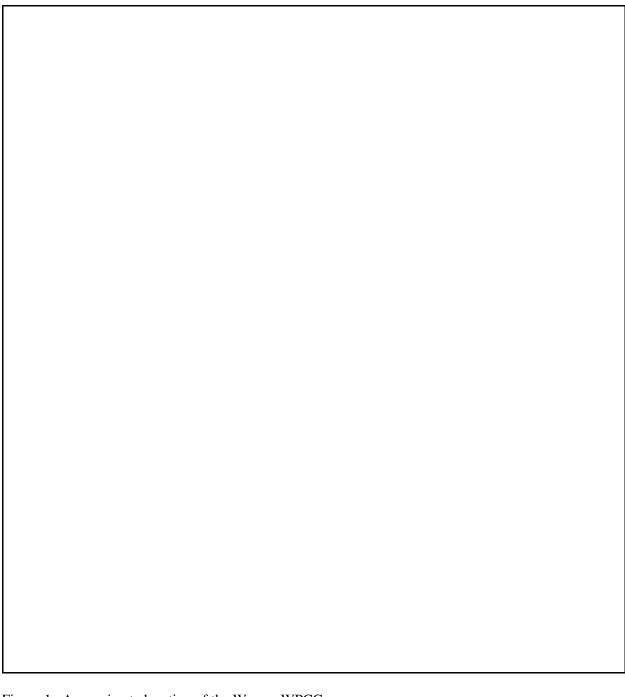
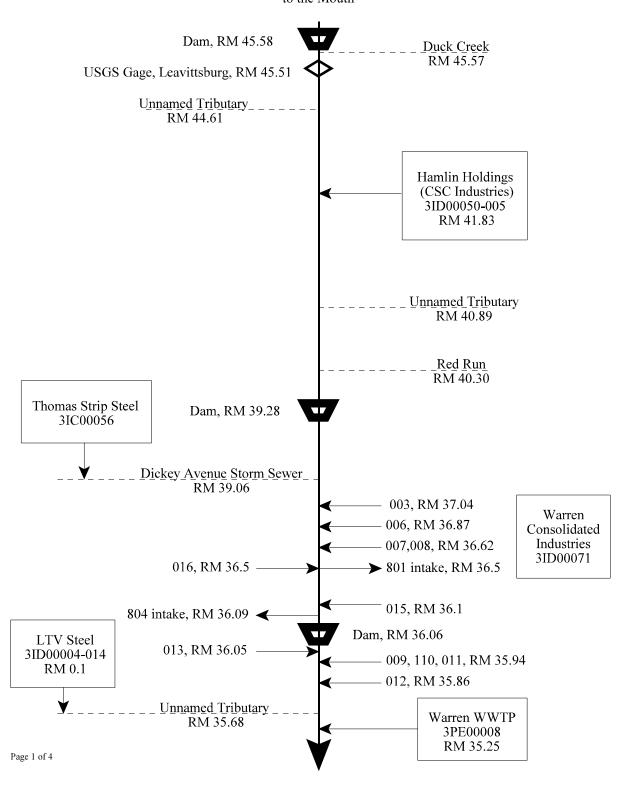
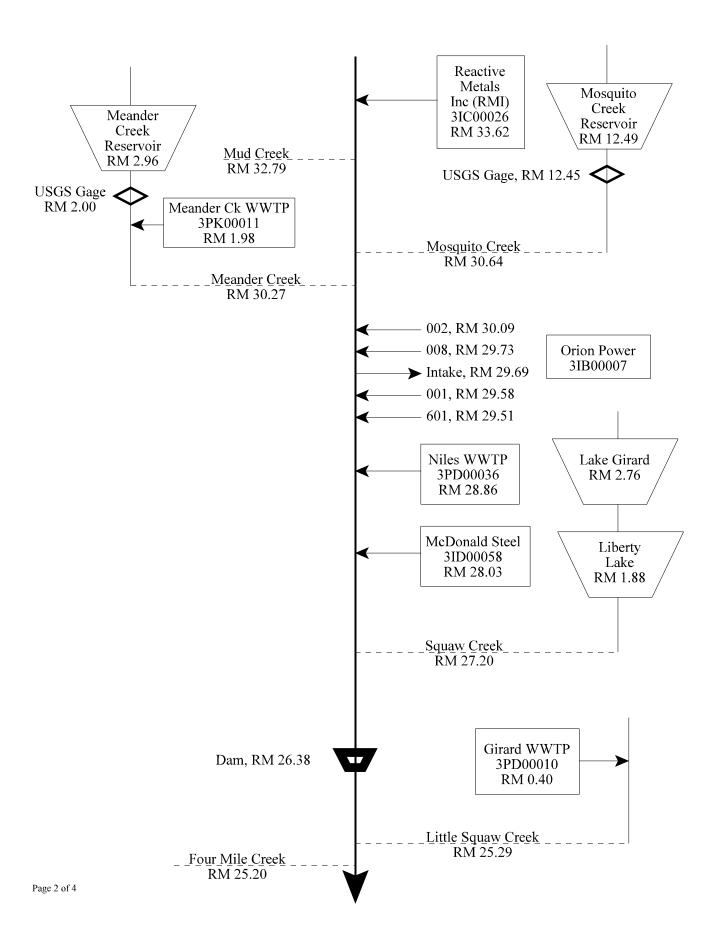


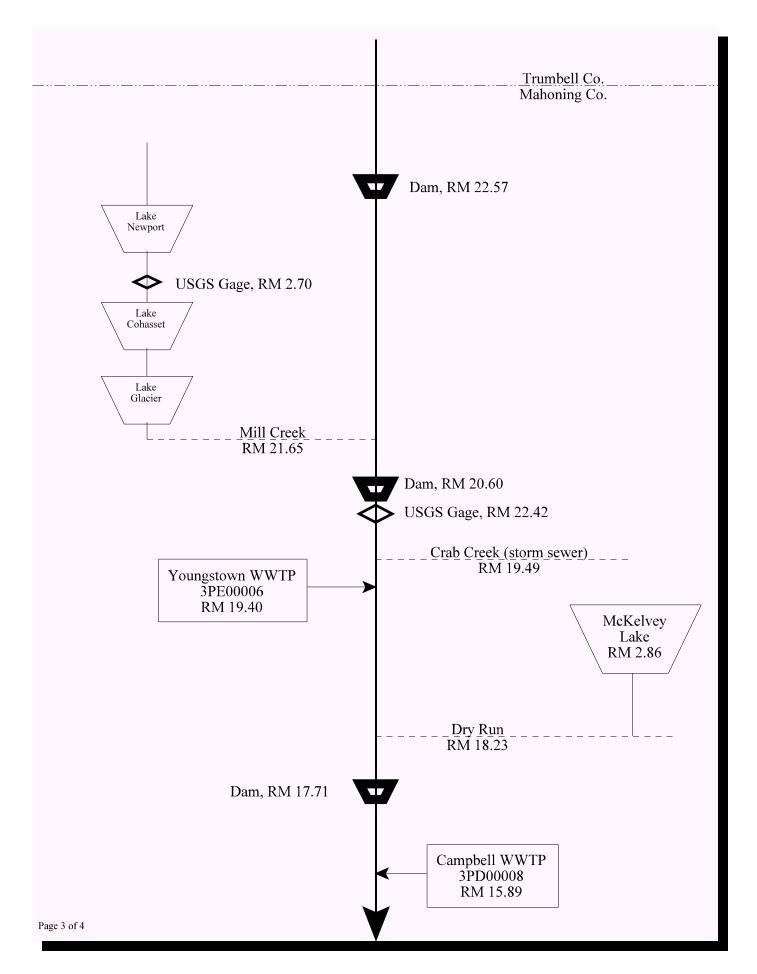
Figure 1. Approximate location of the Warren WPCC.

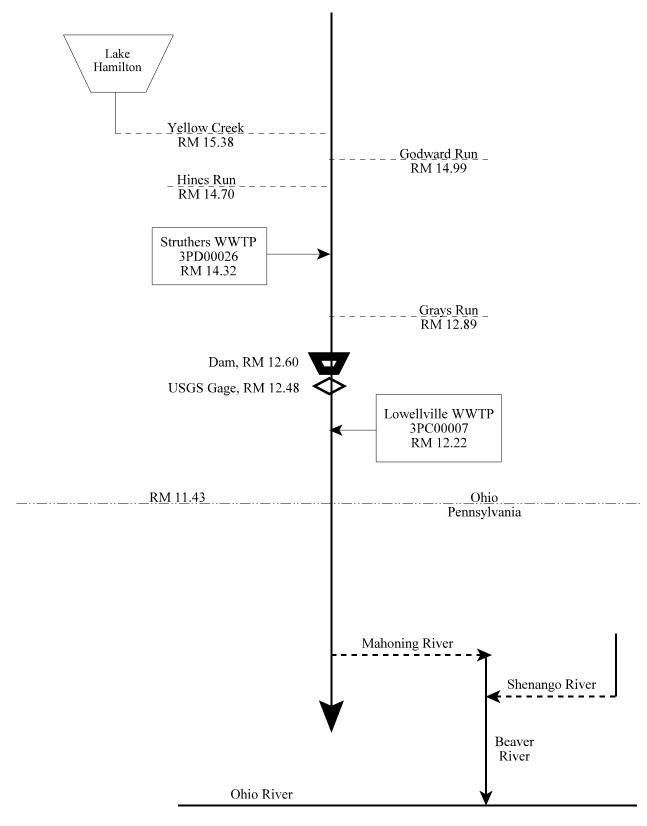
Mahoning River

From Leavittsburg USGS Gage to the Mouth









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